



The Numerical Simulation of Forces with High Angular Speed and Low Angular Acceleration in Three and Five Freedoms of Robotic Arm I

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Abstract

In robot design and application the force and angle with angular speed is important so this study will model numerical simulation and discuss detail data to investigate their property. The force may increase as arm 1 angle increases whilst it may increase if angular speed increases in three freedoms. Meantime it will decrease if angular acceleration increases. It is found that with the angular speed increasing all three force may increase whilst the angular acceleration will cause its increase too in five freedoms. From these value it is observed that F2 is prior one to ensure the strength and fatigue life then F2 is second one to estimate its strength whilst F3 may be neglected. The force may increase as arm 1 angle increases whilst it may increase if angular speed increases in three freedoms. Meantime it will decrease if angular acceleration increases. There is big distance to attain 5KN between the conditions. The effective factor turn to the force is $F1 > F3 > F2$ in three freedoms. The force may increase from 15N to 15KN and 18KN with F3, F2 and F1 in five freedoms. Among them F3 is the least one and F1 is the biggest one. The effect factor turn is $F1 > F2 > F3$. So the F1 and F2 is important one while F3 is neglected. With increasing speed the torque may be decreased and with angular speed becoming big the torque may be increased. The biggest torque is 10KNm and 25KNm when angular speed is 25°/s and 60 °/s respectively. This one needs to be checked the strength correction when the speed is 1m/s. The $\omega_{1\sim3}$ is supposed to be same with ω in addition. The effective turn is $v_2=1\text{m/s} > v_1=10.5\text{m/s} > v_3=1.5\text{m/s}$.

Keywords: Numerical simulation; Force and angle; Angular speed and acceleration; Robotic arm; Angular Acceleration; Three and five freedoms

Introduction

The robotic arm as a new mechanism has been wielded in factory for semi conduction etc. transportation and integration circuit welding. The auto and artificial intelligence robotic arm is developed from experimental lab to factory to launch producing. Therefore grasp the robotic arm kinematic and dynamic will become urgent and necessary in modern society [1-7]. As a multiple system Lagrange equation may be solved its dynamics which is a method currently. Due to its precision demand in process the position defining is very important especially to precise part making. Through defining a route it may be defined a

displacement and then the velocity and acceleration may be defined through the equation besides the force and torque properties. For our checking strength and making size the dynamical properties may be used to it. Such as the motor size and arm shape and size will be checked out to design it. So in this study the dynamic properties may be calculated through Lagrange equation according to kinematic constant to check the feasibility on force to function. To separate three independence parts the velocity and acceleration will be calculated through displacement and force may be computed meantime with Lagrange equation separately. So each resolved resolution may be checked through

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comparing with others and literature. This is the destination in this paper to arouse the further research.

Numerical Simulation

In Figure 1 there are three freedoms in mechanical arm that name as. Meantime there are two other ones call 4&5 which is included The system kinetic energy is [1, 3]

$$E_k = \frac{1}{2} \sum_i^n (m_i v_i^2 + m_i v_i^2 + m_i v_i^2) \quad (1)$$

Here m_i : mass of i component ; J_{si} : rotary inertia of i component relative to center of mass; v_s : center of mass in i component; ω_i : angular velocity in i component; v_1 , v_2 and v_3 is 1,2 and 3 velocities respectively.

$$v_D = \sqrt{\dot{X}_D^2 + \dot{Y}_D^2} \quad (2)$$

From Figure 2 it is known that position coordinate below

$$\begin{cases} X_D = \vec{l}_1 \sin \theta_1 + \vec{l}_2 \sin(\theta_1 + \theta_2) + \vec{l}_3 \sin(\theta_1 + \theta_2 + \theta_3) \\ Y_D = (\vec{l}_1 + \vec{l}_4) \cos \theta_1 + (\vec{l}_2 + \vec{l}_4) \cos(\theta_1 + \theta_2) + (\vec{l}_3 + \vec{l}_4) \cos(\theta_1 + \theta_2 + \theta_3) \end{cases} \quad (3)$$

(3)

Derivating the equation

We gain the \dot{X}_C , \dot{Y}_C , and \dot{X}_3 velocity in hand, $\dot{\theta}_1$, $\dot{\theta}_2$ and $\dot{\theta}_3$ one in joints. Suppose that the acceleration is $\ddot{\theta}_1$, $\ddot{\theta}_2$ and $\ddot{\theta}_3$ and the angular acceleration is $\ddot{\omega}_1$, $\ddot{\omega}_2$ and $\ddot{\omega}_3$ in joints.

$$\begin{cases} \dot{X}_D = \dot{\theta}_1 \vec{l}_1 \cos \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2) \vec{l}_2 \cos(\theta_1 + \theta_2) + (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \vec{l}_3 \cos(\theta_1 + \theta_2 + \theta_3) \\ \dot{Y}_D = \dot{\theta}_1 (\vec{l}_1 + \vec{l}_4) \sin \theta_1 + (\dot{\theta}_1 + \dot{\theta}_2) (\vec{l}_2 + \vec{l}_4) \sin(\theta_1 + \theta_2) + (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) (\vec{l}_3 + \vec{l}_4) \sin(\theta_1 + \theta_2 + \theta_3) \end{cases} \quad (4)$$

V_A , V_B and V_D is B, C and D velocities respectively. So D point velocity is

$$v_D = \sqrt{\dot{X}_D^2 + \dot{Y}_D^2} = \sqrt{l_1^2 \dot{\theta}_1^2 + l_2^2 (\dot{\theta}_1 + \dot{\theta}_2)^2 + l_3^2 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 + \dot{\theta}_1 l_4^2 \sin^2 \theta_1 + l_4^2 (\dot{\theta}_1 + \dot{\theta}_2)^2 \sin^2 (\theta_1 + \theta_2) + l_4^2 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 \sin^2 (\theta_1 + \theta_2 + \theta_3) + 2l_1 l_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_1 + \theta_3) + 2l_2 l_3 (\dot{\theta}_1 + \dot{\theta}_2) (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos \theta_3 + 2l_1 l_4 \dot{\theta}_1 \sin \theta_1 + 2l_2 l_4 (\dot{\theta}_1 + \dot{\theta}_2) \sin(\theta_1 + \theta_2) + 2l_3 l_4 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \sin(\theta_1 + \theta_2 + \theta_3)} \quad (5)$$

C point velocity is

$$v_C = \sqrt{\dot{X}_C^2 + \dot{Y}_C^2} = \sqrt{l_1^2 \dot{\theta}_1^2 + l_2^2 (\dot{\theta}_1 + \dot{\theta}_2)^2 - 2l_1 l_2 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \cos \theta_2} \quad (6)$$

$$v_B = \vec{l}_1 \dot{\theta}_1 \quad (7)$$

Substituting two equations above to equation below

in five freedoms as a rotational and crawling function. In Figure 1 the schematic shows the simplified principle of robot. The coordinate XAY is three freedoms and X'A'Y it five freedoms. In this study the five freedoms not three one is deduced since it is complicated (Figure 1,2).

$$\begin{aligned}
 E_k = & \frac{1}{2} \vec{l}_1 (\vec{l}_1 + \vec{l}_4 + \vec{l}_5) (m_1 + m_2 + m_3) \theta_1^2 + \frac{1}{2} \vec{l}_2 (\vec{l}_2 + \vec{l}_4 + \vec{l}_5) m_2 (\theta_1 + \theta_2)^2 + \frac{1}{2} \vec{l}_2 (\vec{l}_2 + \vec{l}_4 + \vec{l}_5) m_2 (\dot{\theta}_1 + \dot{\theta}_2)^2 \\
 & + \frac{1}{2} \vec{l}_3 (\vec{l}_3 + \vec{l}_4 + \vec{l}_5) m_3 (\theta_1 + \theta_2 + \theta_3)^2 + 2 \vec{l}_4 m_3 \dot{\theta}_1 \sin^2 \theta_2 + \vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2)^2 \sin^2 (\theta_1 + \theta_2) + \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 \\
 & + \dot{\theta}_3)^2 \sin^2 (\theta_1 + \theta_2 + \theta_3) + 2 \vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \cos \theta_2 + \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos (\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 \\
 & + \dot{\theta}_2) (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos \theta_3 + \frac{1}{2} (\vec{l}_4 + \vec{l}_5) (m_1 + m_2 + m_3) \theta_1^2 + \frac{1}{2} (\vec{l}_4 + \vec{l}_5) m_2 (\theta_1 + \theta_2)^2 + \frac{1}{2} (\vec{l}_4 + \vec{l}_5) m_2 (\dot{\theta}_1 + \\
 & \dot{\theta}_2)^2 + 2 \vec{l}_1 \vec{l}_4 m_3 \dot{\theta}_1 \sin (\theta_1 + \theta_2) + 2 \vec{l}_1 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \sin (\theta_1 + \theta_2) + 2 \vec{l}_3 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \sin (\theta_1 + \theta_2 + \theta_3) \quad (8)
 \end{aligned}$$

Here

$$\begin{aligned}
 \frac{\partial E_k}{\partial \dot{\theta}_1} = & (\dot{\theta}_1 + \dot{\theta}_2) \vec{l}_2 m_2 + 2 \vec{l}_4 m_3 \sin^2 \theta_2 + 2 (\dot{\theta}_1 + \dot{\theta}_2)^2 \vec{l}_4 m_3 \sin^2 (\theta_1 + \theta_2) + 2 \\
 & \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \vec{l}_4 m_3 \sin^2 (\theta_1 + \theta_2) + 2 \vec{l}_4 m_3 \sin^2 (\theta_1 + \theta_2 + \theta_3) + 2 (\dot{\theta}_1 + \dot{\theta}_2) \vec{l}_1 \vec{l}_2 \\
 & m_2 \cos \theta_2 + 2 \dot{\theta}_1 \vec{l}_1 \vec{l}_2 m_2 \cos \theta_2 + \dot{\theta}_1 \vec{l}_1 \vec{l}_2 m_3 \cos (\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \\
 & \dot{\theta}_3) \cos (\theta_1 + \theta_2 + \theta_3) + \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \cos \theta_3 + \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos \theta_3 \\
 & + 2 \vec{l}_1 \vec{l}_4 m_3 \sin (\theta_1 + \theta_2) + 2 \vec{l}_1 \vec{l}_4 m_3 \sin (\theta_1 + \theta_2) + 2 \vec{l}_1 \vec{l}_4 m_3 \cos (\theta_1 + \theta_2 + \theta_3) \quad (9)
 \end{aligned}$$

$$\begin{aligned}
 \frac{\partial E_k}{\partial \dot{\theta}_2} = & \vec{l}_2 m_2 (\dot{\theta}_1 + \dot{\theta}_2) + \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2)^2 \sin^2 (\theta_1 + \theta_2) + 2 \vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \sin \\
 & ^2 (\theta_1 + \theta_2) + 2 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \sin^2 (\theta_1 + \theta_2) + 2 \vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1 \cos \theta_2 + \vec{l}_1 \vec{l}_2 m_2 \\
 & (\dot{\theta}_1 + \dot{\theta}_2) \cos \theta_2 + \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) + \cos (\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \\
 & \cos \theta_3 + \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \cos \theta_3 + 2 \vec{l}_1 \vec{l}_4 m_3 \sin (\theta_1 + \theta_2) + 2 \vec{l}_1 \vec{l}_4 m_3 \sin (\theta_1 + \theta_2 \\
 & + \theta_3) \quad (10)
 \end{aligned}$$

$$\begin{aligned}
 \frac{\partial E_k}{\partial \dot{\theta}_3} = & \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 \cos (\theta_1 + \theta_2 + \theta_3) + 2 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \sin^2 (\theta_1 + \theta_2 + \\
 & \theta_3) + \vec{l}_1 \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos (\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 \cos (\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m \\
 & _3 (\dot{\theta}_1 + \dot{\theta}_2) \cos \theta_3 + \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 \cos (\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_3) \cos \theta_3 + 2 \vec{l}_1 \vec{l}_4 \\
 & m_3 \cos (\theta_1 + \theta_2 + \theta_3) \quad (11)
 \end{aligned}$$

And

$$\begin{aligned}
 \frac{d}{dt} \left(\frac{\partial E_K}{\partial \dot{\theta}_1} \right) &= \vec{l}_2 m_2 (\ddot{\theta}_1 + \ddot{\theta}_2) + 4(\ddot{\theta}_1 + \ddot{\theta}_2) \dot{\theta}_2 \vec{l}_1 \vec{l}_2 m_2 \sin \theta_2 \cos \theta_2 + 4(\dot{\theta}_1 \\
 &+ \dot{\theta}_2) \vec{l}_4 m_3 \sin^2(\theta_1 + \theta_2) + 4(\dot{\theta}_1 + \dot{\theta}_2)^3 \vec{l}_4 m_3 \cos(\theta_1 + \theta_2) + 2(\dot{\theta}_1 + \dot{\theta}_2) \vec{l}_4 \\
 &m_3 \sin^2(\theta_1 + \theta_2) + 4(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \vec{l}_4 m_3 \sin(\theta_1 + \theta_2 + \theta_3) - 2\dot{\theta}^2 \vec{l}_1 \vec{l}_2 m_2 \sin \theta_2 - 2 \\
 &(\dot{\theta}_1 + \dot{\theta}_2) \dot{\theta}_2 \vec{l}_1 \vec{l}_2 m_2 \sin \theta_1 + 2\ddot{\theta} \vec{l}_1 \vec{l}_2 m_2 \cos \theta_2 - 2\dot{\theta}^2 \vec{l}_1 \vec{l}_2 m_2 \sin \theta_2 + \ddot{\theta} \vec{l}_1 \vec{l}_2 m_3 \\
 &\cos(\theta_1 + \theta_2) - \dot{\theta}_1 \vec{l}_1 \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \sin(\theta_1 + \theta_2) + \vec{l}_2 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) \cos(\theta_1 + \theta_2) \\
 &+ \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) (\dot{\theta}_1 + \dot{\theta}_2) \cos(\theta_1 + \theta_2) + \vec{l}_2 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2) \cos \theta_3 + \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \\
 &\dot{\theta}_3 \cos \theta_3 + \vec{l}_1 \vec{l}_2 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) \cos \theta_3 + \vec{l}_2 \vec{l}_3 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) \cos \theta_3 + \vec{l}_2 \vec{l}_3 m_3 \\
 &(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \dot{\theta}_3 + 4(\ddot{\theta}_1 + \ddot{\theta}_2) \vec{l}_1 \vec{l}_4 m_3 \cos(\theta_1 + \theta_2) + 2(\dot{\theta}_1 + \dot{\theta}_2)^3 \vec{l}_1 \vec{l}_4 m_3 \cos(\theta_1 + \theta_2) \\
 &- 2(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \vec{l}_1 \vec{l}_4 m_3 \sin(\theta_1 + \theta_2 + \theta_3)
 \end{aligned} \tag{12}$$

$$\begin{aligned}
 \frac{d}{dt} \left(\frac{\partial E_K}{\partial \dot{\theta}_2} \right) &= \vec{l}_2 m_2 (\ddot{\theta}_2 + \ddot{\theta}_1) + 2\vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2) (\ddot{\theta}_2 + \ddot{\theta}_1) \sin^2(\theta_1 + \theta_2) - 4\vec{l}_4 m_3 (\dot{\theta}_1 \\
 &+ \dot{\theta}_2)^2 (\ddot{\theta}_2 + \ddot{\theta}_1) \sin(\theta_1 + \theta_2) \cos(\theta_1 + \theta_2) + 2\vec{l}_4 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) (\dot{\theta}_1 + \dot{\theta}_2) \sin^2(\theta_1 \\
 &+ \theta_2) + 2\vec{l}_4 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2) \sin^2(\theta_1 + \theta_2) - 4\vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2)^2 \sin(\theta_1 + \theta_2) \cos(\theta_1 + \\
 &\theta_2) + 2\vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 \cos \theta_2 + 2\vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1 \dot{\theta}_2 \cos \theta_2 + \vec{l}_1 \vec{l}_2 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2) \cos(\theta_1 + \theta_2) \\
 &- \vec{l}_1 \vec{l}_2 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) (\dot{\theta}_1 + \dot{\theta}_2) \sin(\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) \cos \theta_1 - \vec{l}_1 \vec{l}_2 \\
 &m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \dot{\theta}_1 \sin \theta_1 + \vec{l}_2 \vec{l}_3 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) \cos \theta_3 + 2\vec{l}_1 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \cos(\theta_1 \\
 &+ \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_1 + \theta_2 + \theta_3)
 \end{aligned} \tag{13}$$

$$\begin{aligned}
 \frac{d}{dt} \left(\frac{\partial E_K}{\partial \dot{\theta}_3} \right) &= \vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) + 2\vec{l}_4 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) \sin^2(\theta_1 + \theta_2 + \theta_3) + \\
 &4\vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 \sin(\theta_1 + \theta_2 + \theta_3) \cos(\theta_1 + \theta_2 + \theta_3) - \vec{l}_1 \vec{l}_2 m_3 (\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3) (\dot{\theta}_1 + \dot{\theta}_2) \\
 &\sin(\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 \cos(\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 \cos(\theta_1 + \theta_2) + \vec{l}_3 \vec{l}_2 m_3 \\
 &(\ddot{\theta}_1 + \ddot{\theta}_3) \cos \theta_3 - \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_3) \dot{\theta}_3 \sin \theta_3 - \vec{l}_1 \vec{l}_4 m_3 \cos(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)
 \end{aligned} \tag{14}$$

$$\begin{aligned}
 \frac{\partial E_K}{\partial \theta_1} &= \vec{l}_1 (\vec{l}_1 + \vec{l}_4 + \vec{l}_5) (m_1 + m_2 + m_3) \theta_1 + \vec{l}_2 (\vec{l}_3 + \vec{l}_4 + \vec{l}_5) m_2 (\theta_1 + \theta_2) + \vec{l}_3 (\vec{l}_3 + \vec{l}_4 + \vec{l}_5) m_3 (\theta_1 + \theta_2 + \theta_3) \\
 &+ 2\vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2)^2 \sin(\theta_1 + \theta_2) - 2\vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 \sin(\theta_1 + \theta_2 + \theta_3) - \vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \sin \\
 &(\theta_1 + \theta_2) + (\vec{l}_4 + \vec{l}_5) (m_2 + m_2 + m_3) \theta_1 + (\vec{l}_4 + \vec{l}_5) m_2 (\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \cos(\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 \\
 &(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_1 + \theta_2)
 \end{aligned} \tag{15}$$

$$\begin{aligned} \frac{\partial E_k}{\partial \theta_2} = & \vec{l}_2 (\vec{l}_2 + \vec{l}_4 + \vec{l}_5) m_2 (\dot{\theta}_1 + \dot{\theta}_2) + \vec{l}_3 (\vec{l}_3 + \vec{l}_4 + \vec{l}_5) m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) + 4\vec{l}_4 m_3 \dot{\theta}_1 \sin \theta_2 + 2\vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2)^2 \sin \\ & (\theta_1 + \theta_2) + 2\vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 \sin(\theta_1 + \theta_2 + \theta_3) - 2\vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \sin \theta_2 - 2\vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \sin \theta_2 - (\vec{l}_4 \\ & + \vec{l}_5) m_3 \dot{\theta}_1 (\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_1 + \theta_2) - (\vec{l}_4 + \vec{l}_5) m_3 \dot{\theta}_1 (\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 \dot{\theta}_1 \cos(\theta_1 + \theta_2) + \\ & 2\vec{l}_3 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_1 + \dot{\theta}_2) \cos(\theta_1 + \theta_2 + \theta_3) \end{aligned} \quad (16)$$

$$\begin{aligned} \frac{\partial E_k}{\partial \theta_3} = & \vec{l}_3 (\vec{l}_3 + \vec{l}_4 + \vec{l}_5) (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) - 2\vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)^2 \sin(\theta_1 + \theta_2 + \theta_3) - \vec{l}_2 \vec{l}_3 m_3 (\dot{\theta}_1 + \dot{\theta}_2) \\ & (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \sin \theta_3 - 2\vec{l}_3 \vec{l}_4 m_3 (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \cos(\theta_1 + \theta_2 + \theta_3) \end{aligned} \quad (17)$$

Potential energy of System

$$E_p = (\vec{l}_1 + \vec{l}_4) m_1 g \cos \theta_1 + (\vec{l}_2 + \vec{l}_4) m_2 g \cos(\theta_1 + \theta_2) + (\vec{l}_3 + \vec{l}_4) m_3 g \cos(\theta_1 + \theta_2 + \theta_3) \quad (18)$$

$$\frac{\partial E_p}{\partial \theta_1} = \vec{l}_1 \vec{l}_4 m_1 g \dot{\theta}_1 \sin \theta_1 \quad (19)$$

$$\frac{\partial E_p}{\partial \theta_2} = \vec{l}_2 \vec{l}_4 m_2 g \dot{\theta}_2 \sin(\theta_1 + \theta_2)$$

$$\frac{\partial E_p}{\partial \theta_3} = \vec{l}_3 \vec{l}_4 m_3 g \dot{\theta}_3 \sin(\theta_1 + \theta_2 + \theta_3)$$

Substituting Lagrange equation below (10) for above equations

Lagrange equation is

$$\frac{d}{dt} \left(\frac{\partial E_k}{\partial \dot{q}_i} \right) - \frac{\partial E_k}{\partial q_i} + \frac{\partial E_p}{\partial q_i} = F_i \quad (20)$$

Here E_k is kinetic of system;

E_p is potential energy of system;

q_i is generalized coordinate, it is a group of independent parameters that can define mechanical system movement;

F_i is generalized force, when q_i is a angular displacement it a torque, when q_i is linear displacement it a force;

n is system generalized coordinate.

System generalized force

Supposed that $F_k(k=1,2,\dots,m)$ and $M_j(j=1,2,\dots,n)$ is force and torque acting on system. Its power is

$$P = \sum_{k=1}^m (F_k v_k \cos \alpha_k) + \sum_{j=1}^n (\pm M_j \omega_j) \quad (21)$$

Here ω_j : angular velocity acting on component with M_j ;

V_K : The velocity in force F_k point of action; (the syntropy +, reverse direction -)

α_K : Angle between F_K and V_K

When generalized coordinates is φ angular displacement generalized force=equivalent torque

$$\delta W_2 = \sum_{k=1}^m (F_k \delta v_k \cos \alpha_k) + \sum_{j=1}^n (\pm M_j \delta \omega_j) \quad (22)$$

Here α_K is zero; $F_K = 200N$; $V_K = 0.2 \sim 0.3m/s$; $\dot{\theta} = 20 \sim 30^\circ/s = 20 \sim 30Nm$. is $\delta \varphi_j$ virtual angular displacement; δs_k is virtual displacement.

Supposing that

$$\delta s_k = \frac{\partial s_k}{\partial q_1} \delta q_1 + \frac{\partial s_k}{\partial q_2} \delta q_2 \quad (23)$$

$$\delta \varphi_k = \frac{\partial \varphi_j}{\partial q_1} \delta q_1 + \frac{\partial \varphi_j}{\partial q_2} \delta q_2 \quad (24)$$

Replace equation below with above two equations

$$\begin{cases} F_1 = \sum_{k=1}^m \left[F_k \frac{\partial s_k}{\partial q_1} \cos \alpha_k \right] + \sum_{j=1}^n \left[M_j \frac{\partial \varphi_j}{\partial q_1} \right] \\ F_2 = \sum_{k=1}^m \left[F_k \frac{\partial s_k}{\partial q_2} \cos \alpha_k \right] + \sum_{j=1}^n \left[M_j \frac{\partial \varphi_j}{\partial q_2} \right] \end{cases} \quad (25)$$

This is generalized force equation.

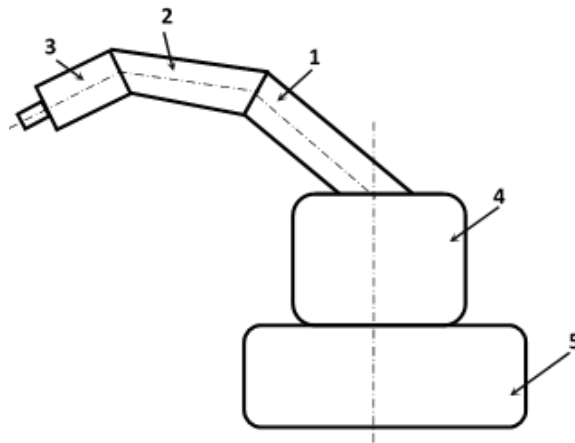


Figure 1: Construction schematic of mechanical arm in series in robot 3-hand part; 2-wrist part; 1-arm part; 4-waist part; 5-two crawling wheel.

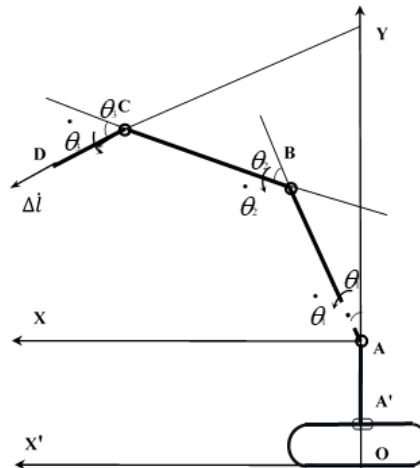
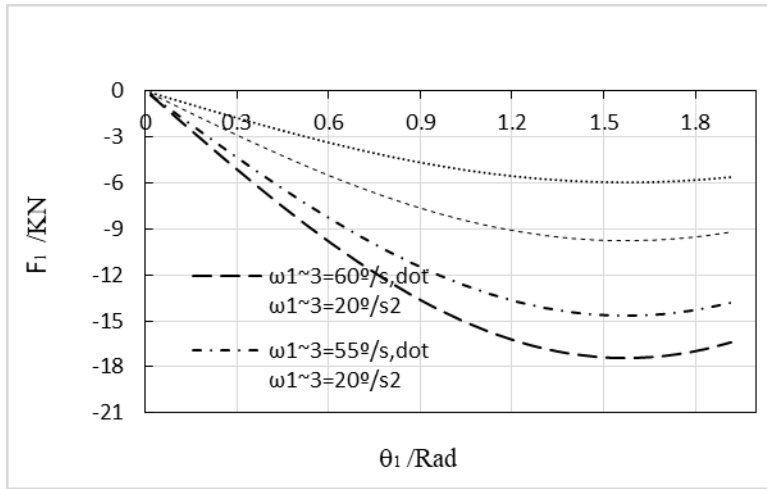
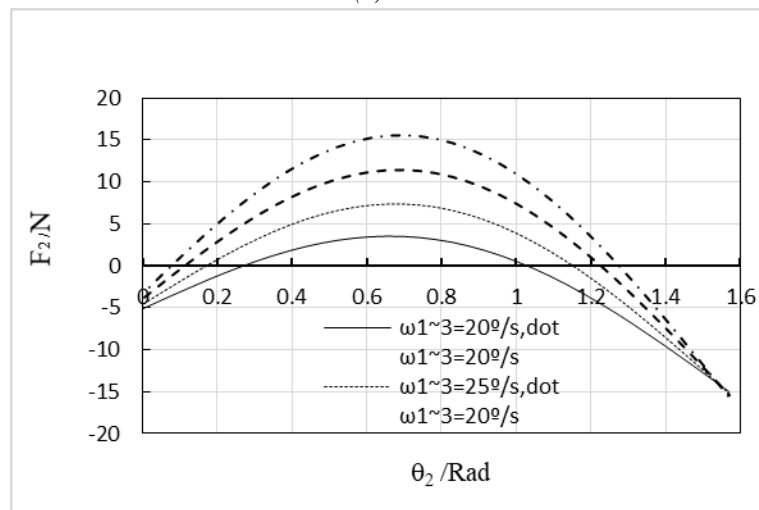


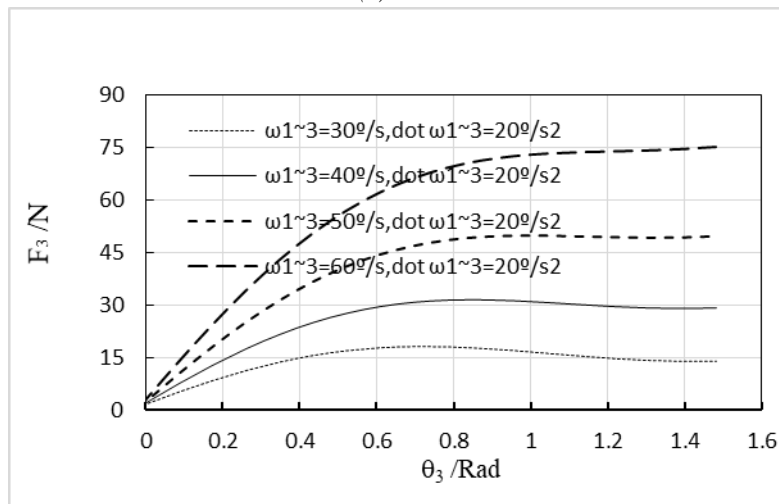
Figure 2: Principle schematic of mechanical arm in series in robot.



(a) F1



(b) F2.



(c) F3.

Figure 3: The curve of force and angle with various angular speed and acceleration at angular acceleration of $20^\circ/s^2$ in three freedoms of robot arm.

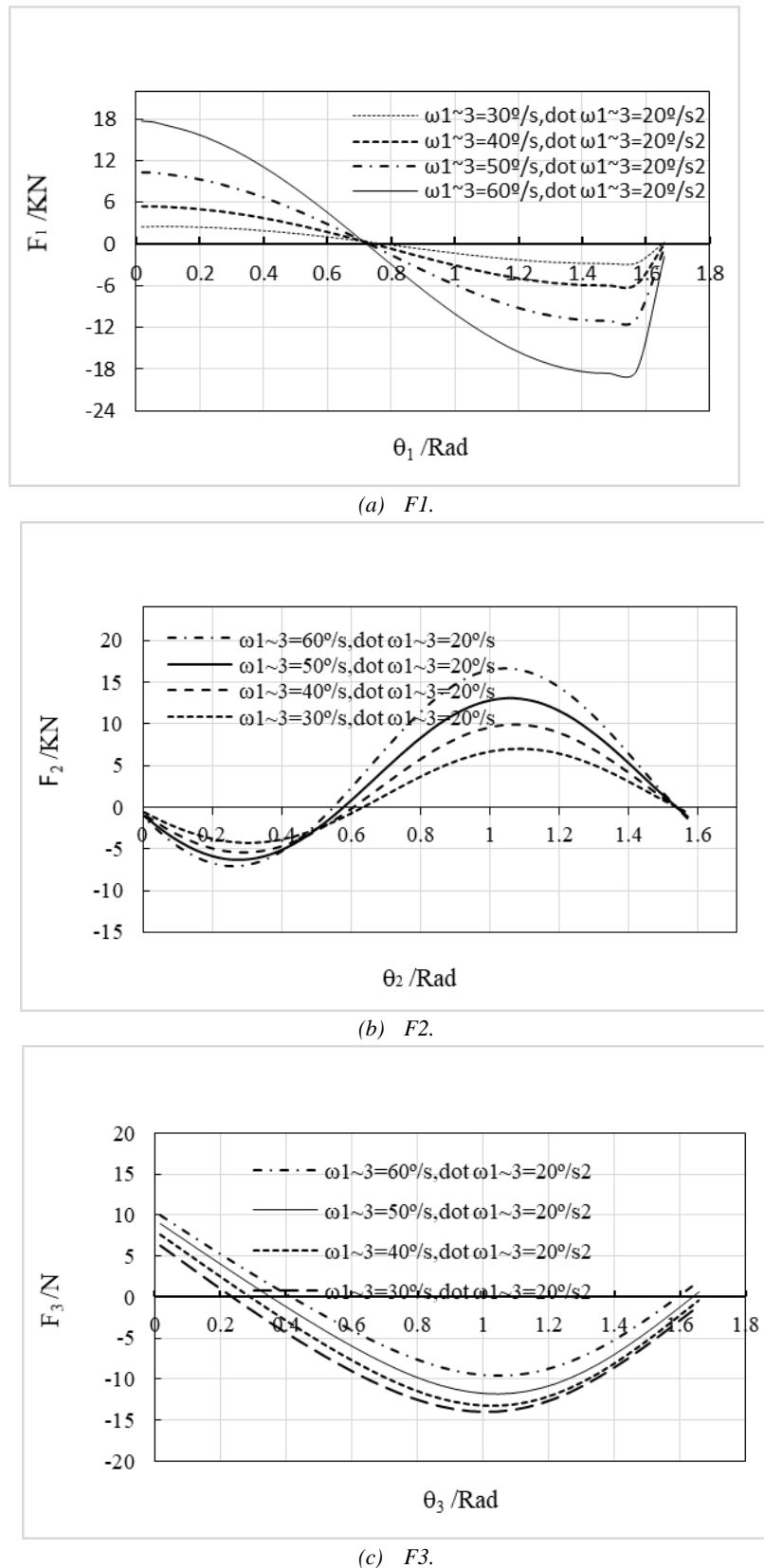
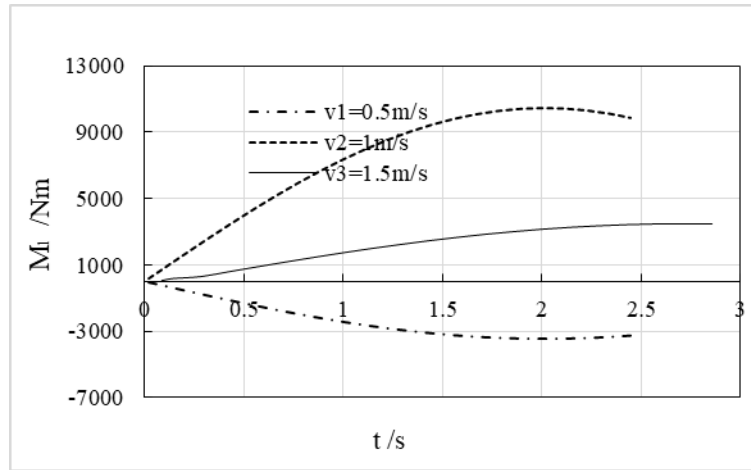
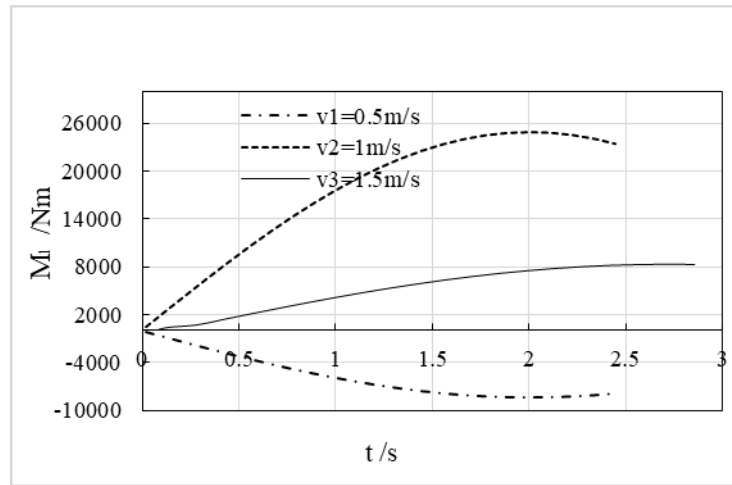


Figure 4: The curve of force and angle with various angular speed and acceleration at angular acceleration of $20^\circ/s^2$ in five freedoms of robot arm.



(a) $\omega=25^\circ/s$.



(b) $\omega=60^\circ/s$.

Figure 5: The torque with time and speed v under angular speed ω and acceleration ω' of $20^\circ/s^2$.

Table 1: Parameters of robot arms.

items	Value	Item	Value
l1 /m	0.55	$\dot{\theta}_1 /^\circ/s$	30~60
l2 /m	0.5	$\dot{\theta}_2 /^\circ/s$	30~60
l3 /m	0.3	$\dot{\theta}_3 /^\circ/s$	30~60
m1/N	7.7	$\ddot{\theta}_1 /^\circ/s^2$	20
m2/N	6.6	$\ddot{\theta}_2 /^\circ/s^2$	20
m3/N	4.0	$\ddot{\theta}_3 /^\circ/s^2$	20

Discussions

As seen in Table 1 the parameter in robot arm is listed. [6~7] Here $\theta_1, \theta_2, \theta_3$ is the arm1, arm2, arm3 angle respectively. l_1, l_2, l_3 is arm length. m_1, m_2, m_3 is arm mass. Number is arm label. According to these parameters the below curves are gained as

below in Figure 3 &4. As seen in Figure 3(a~c) the force of arm1 will increase with the angular speed and acceleration increasing that expresses the proportional relation between them fitting to Newton theory well. That says that angular speed raises the acceleration meantime the later raise the force too. They all distributes into sinusoidal continuous wave that forms semiwave



with 90° . The force may increase from 15N to 15KN and 18KN with F3, F1 and F2 as seen in Figure 4. Among them F3 is the least one and F1 is the biggest one. The effect factor turn is $F1 > F2 > F3$ at the angular acceleration of $20^\circ/s^2$. So the F1 is important one attained 1.8Tons and F2 is second attains 1.5tons while F3 is neglected. From these value it is observed that F1 is prior one to ensure the strength and fatigue life then F2 is second one to estimate its strength whilst F3 may be neglected in five freedoms. In contrast to above in Figure 3 in three freedoms the force F1 is about 18KN ie. 1.8tons which is the biggest need to be checked the strength estimation and then F3 is 75N and at last F2 is 16N which are neglected here. The effect turn is $F1 > F3 > F2$ (Table 1).

As seen in Figure 3 the force may increase as arm 1 angle increases whilst it may increase if angular speed increases in three freedoms. Meantime it will decrease if angular acceleration increases in Figure 3(d). The maximum is 18KN in Figure 3(a) if angular speed is $20^\circ/s$ and acceleration is $20^\circ/s^2$ so this point will be checked to ensure the robotic arm strength. There is big distance to attain 3~5KN between the conditions. The effective factor turn to the force is $F1 > F3 > F2$ in three freedoms (Figure 3). In the modelling of five freedoms in movement of robotic arm the kinetic equation is established according to Lagrange formula based on three freedoms robotic arm. It compensates the blank in four freedoms and one impulsion on robot. It is found that the first and second solution is complicated and long the whole equations is concise than the traditional equation. This is a blank in five freedoms which can shorten the whole numerical computation a lot. Referring to the important occasion the kinetic equation will only be computed on three freedoms according to this study (Figure 4).

It is suggested that the big arm happens when angular speed and acceleration is big. So that the reasonable parameters are chosen to design and estimate their properties is important. Not to choose big angular speed and acceleration is key in order to increase the capability and property that may increase the whole cost as well (Figure 5).

Overview the computation is shorter than the five freedoms traditional one. The solution is easy to use in software like Excel and Origin. The result is satisfactory and precise to be adopted to numerical simulation so the five freedoms method based on three freedoms is feasible. In Figure 5 with increasing speed the torque may be decreased and with angular speed becoming big the torque may be increased. The biggest torque is 10KNm and 25KNm when angular speed is $25^\circ/s$ and $60^\circ/s$ respectively. This one needs to be checked the strength correction when the speed is 1m/s. The ω_{1-3} is supposed to be same with angular speed ω and angular acceleration ω' of $20^\circ/s^2$ in Figure 5 in addition. The effective turn is $v_2=1m/s > v_1=10.5m/s > v_3=1.5m/s$.

Conclusions

- There is big distance to attain 5KN between the conditions. The effective factor turn to the force is $F1 > F3 > F2$ in three freedoms.
- The force may increase from 15N to 15KN and 18KN with F3, F2 and F1 in five freedoms. Among them F3 is the least one and F1 is the biggest one. The effect factor turn is $F1 > F2 > F3$. so the F1 and F2 is important one while F3 is neglected.

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